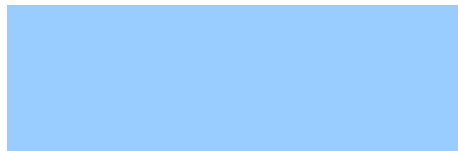


# Antenna FM transmitter



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mw.uos.ac.kr

## • : FM transmitter

- 1) discrete BJT
- 2) BJT
- 3) Oscillator
- 4) Monopole
- 5) Frequency Modulator
- 6) microphone
- 6)

FM 1 (5/09): BJT

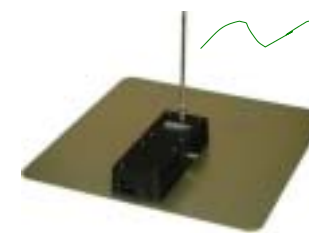
FM2 (5/16):

FM3 (5/22):

FM transmitter

FM4 (6/05): FM transmitter

FM transmitter



Radio



## FM2: Colpitts

- 1) Monopole
- 2) Frequency Modulator
- 3) microphone

- PSPI CE (Pre-Report)

- 2N2222 2 :

- Microphone

- 가

-

- ( 0.8mm 20cm)

- 470 pF 3 , 4.7uF 2 , 4.7 pF 2 , 10k 2 , 100k2

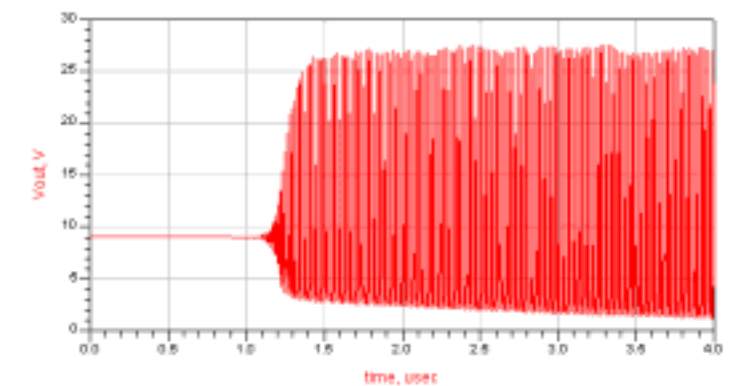
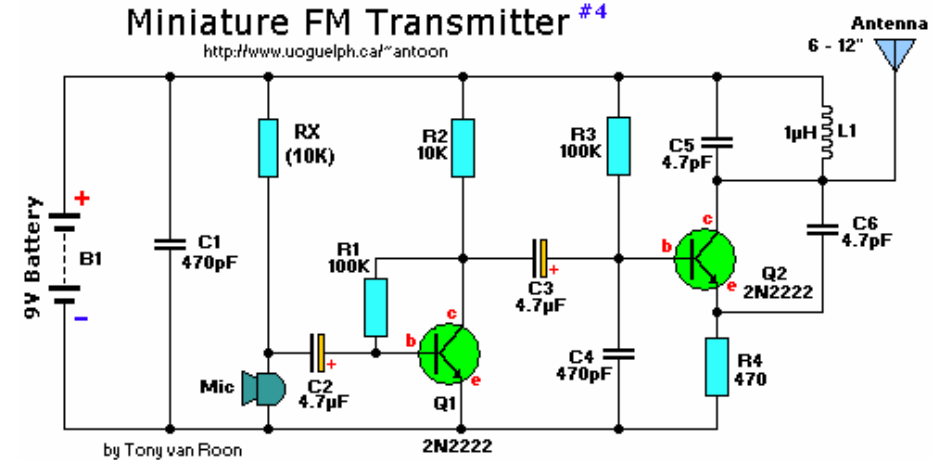
-

- air-coil

- Radio

## Miniature FM Transmitter #4

<http://www.uoguelph.ca/~antoon>



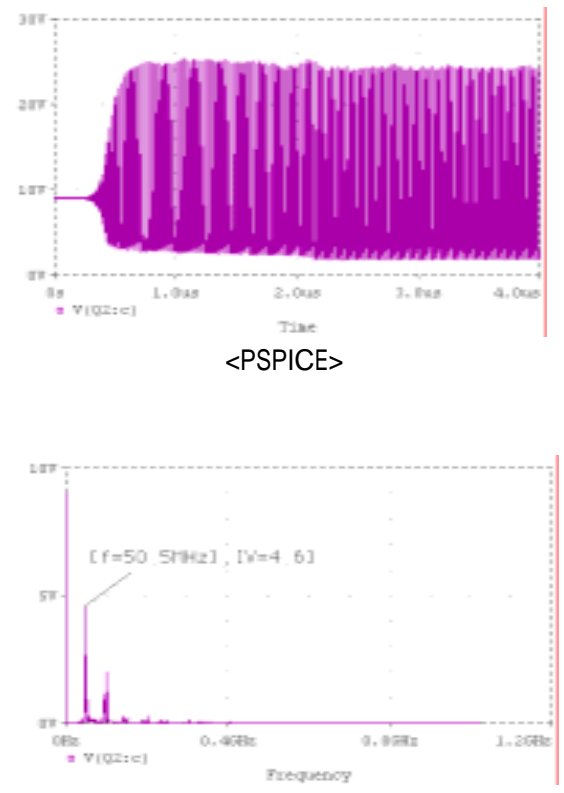
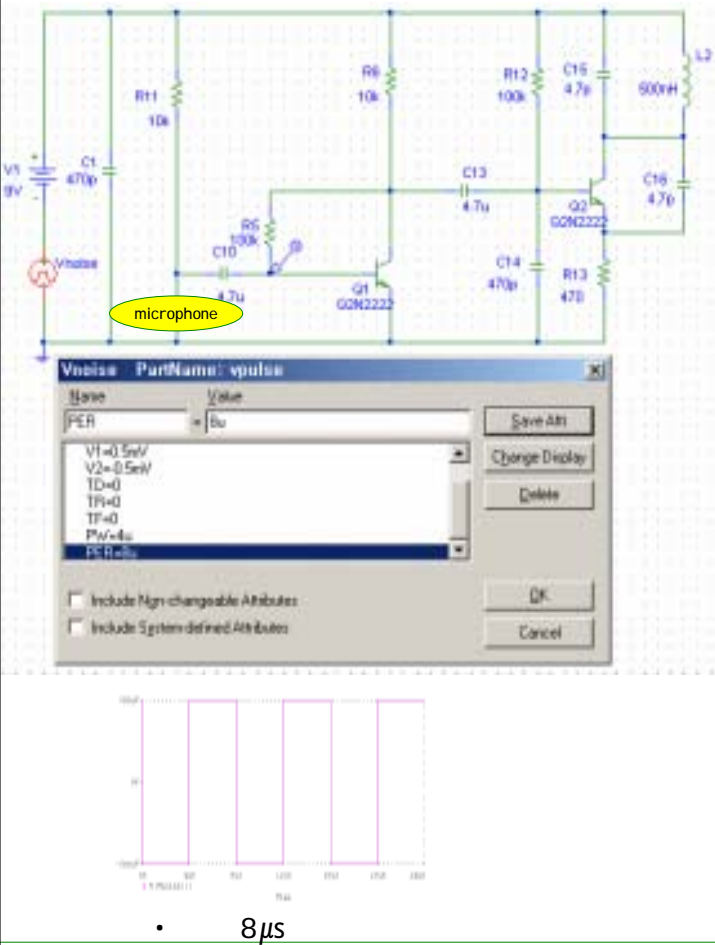


TABLE 7-5 Band Designations for Microwave Frequency Ranges

Old <sup>†</sup>	New	Frequency Ranges (GHz)
Ka	K	26.5–40
K	K	20–26.5
K	J	18–20
Ku	J	12.4–18
X	J	10–12.4
X	I	8–10
C	H	6–8
C	G	4–6
S	F	3–4
S	E	2–3
L	D	1–2
UHF	C	0.5–1

<sup>†</sup> Because the old band designations have been in wide use since the early days of radar, they are still in common use because of habit.

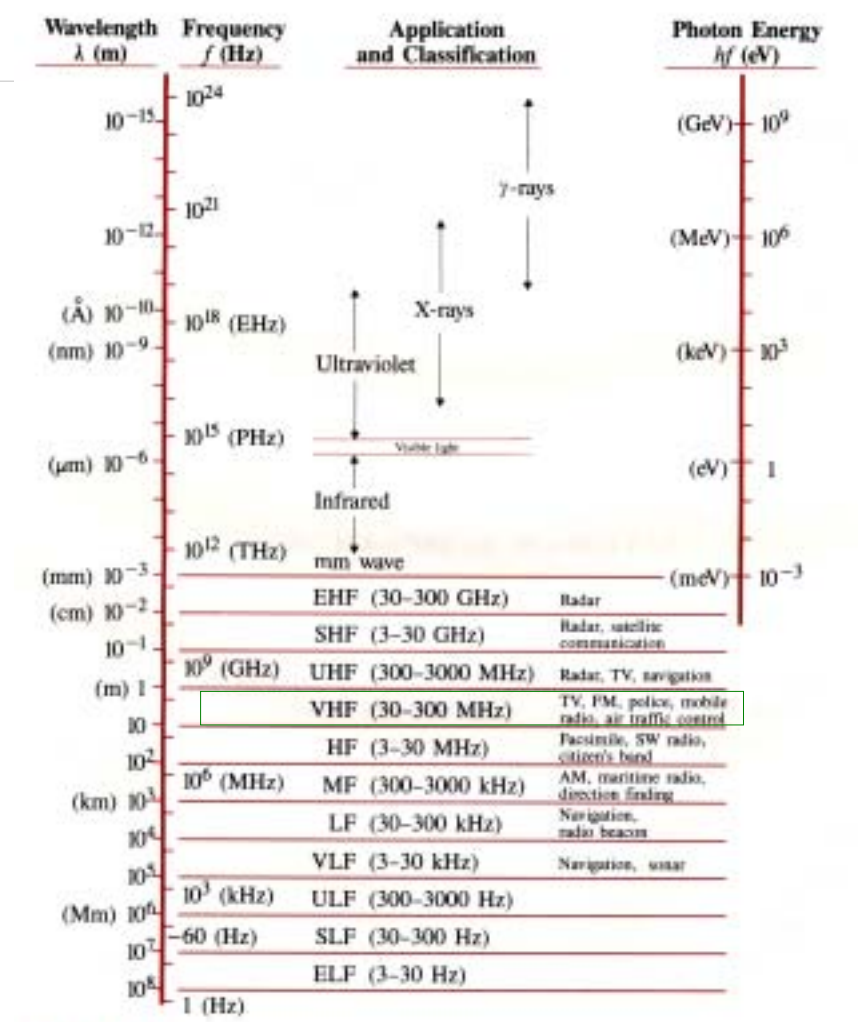
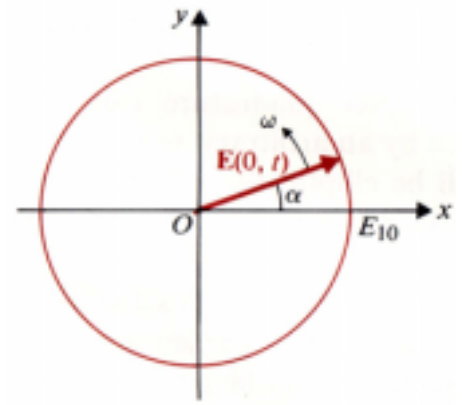


FIGURE 7-9 Spectrum of electromagnetic waves.

Polarization of Plane Waves

$$\mathbf{E}(0, t) = \mathbf{a}_x E_1(0, t) + \mathbf{a}_y E_2(0, t)$$

$$= \mathbf{a}_x E_{10} \cos \omega t + \mathbf{a}_y E_{20} \sin \omega t.$$



$E_{20} = E_{10}$

$$\alpha = \tan^{-1} \frac{E_2(0, t)}{E_1(0, t)} = \omega t$$

E-field rotates at a uniform rate with in a counterclockwise direction → right-handed, or positive circularly polarized wave (RHCP)

$$\mathbf{E}(z) = \mathbf{a}_x E_{10} e^{-jkz} + \mathbf{a}_y j E_{20} e^{-jkz}$$

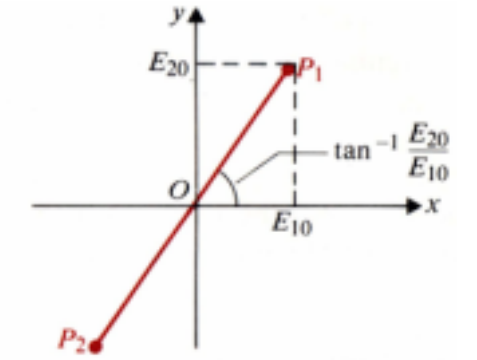
$$\mathbf{E}(0, t) = \mathbf{a}_x E_{10} \cos \omega t - \mathbf{a}_y E_{20} \sin \omega t.$$

left-handed, negative circularly polarized wave (LHCP)

Polarization of Plane Waves

$$\mathbf{E}(0, t) = (\mathbf{a}_x E_{10} + \mathbf{a}_y E_{20}) \cos \omega t.$$

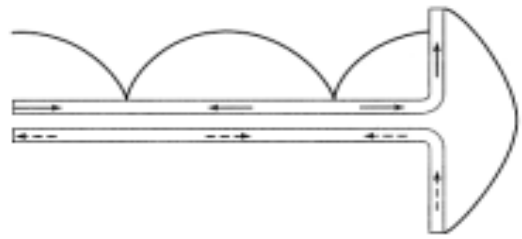
→ linearly polarized wave



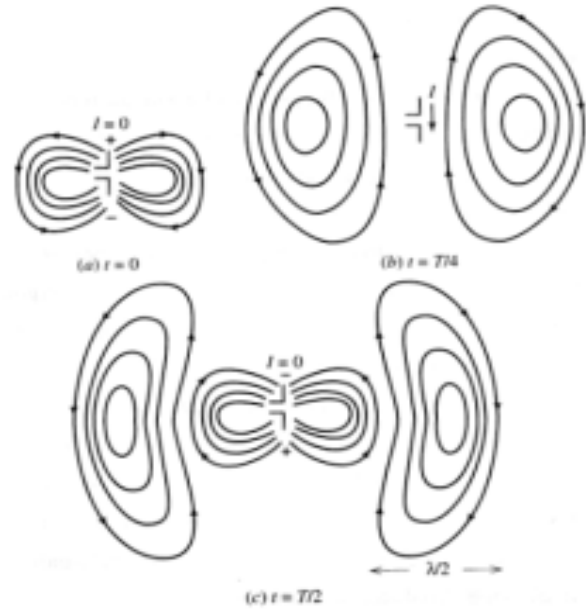
applications of polarization

- AM broadcast stations : linearly polarized with the E-field perpendicular to the ground
- TV broadcast stations : linearly polarized in the horizontal direction
- FM broadcast stations : circularly polarized





•Two-wire



• (electric field line)

-  $F(\theta, \phi)$  : (radiation)  
 (narrow beam)

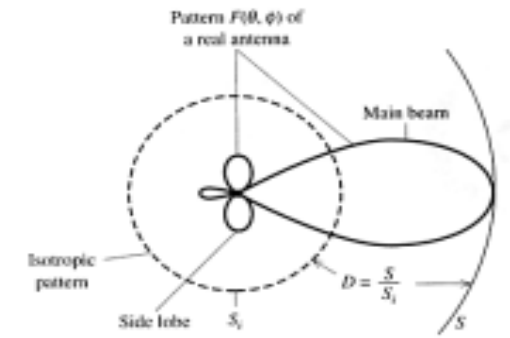
- D :

- G :

- :

-  $Z_A$  :

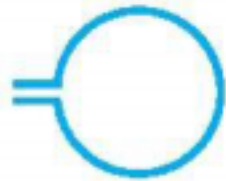
- :



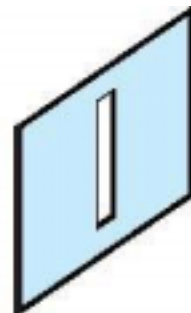
monopole



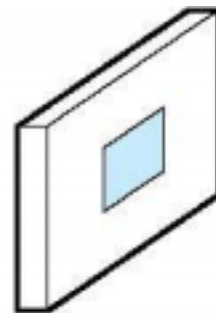
Dipole



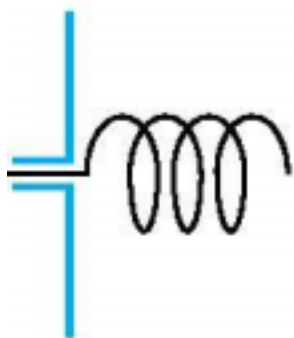
Loop



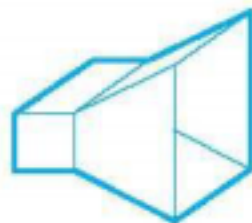
Slot



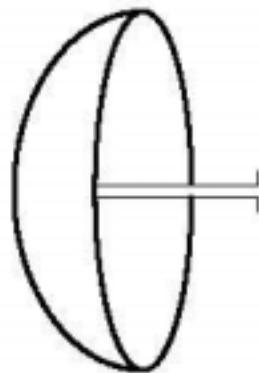
Patch



Helical

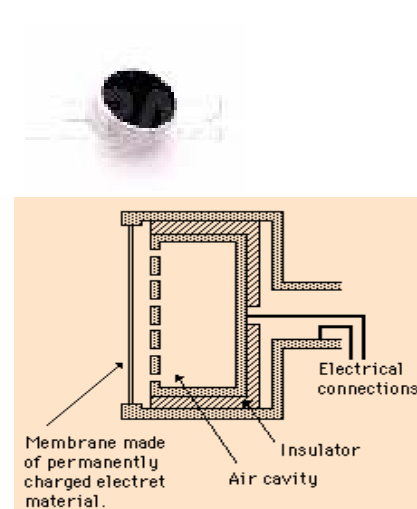


Horn



Reflector

### Condenser Microphone



$$C = \frac{q}{v} = \epsilon \frac{S}{d} \quad v = \frac{q}{\epsilon S}$$

$$v' = \frac{q}{\epsilon S} (d + \Delta d) = \frac{q}{\epsilon S} d + \frac{q}{\epsilon S} \Delta d = v + \Delta v$$

$$\Delta v = \frac{q}{\epsilon S} \Delta d$$

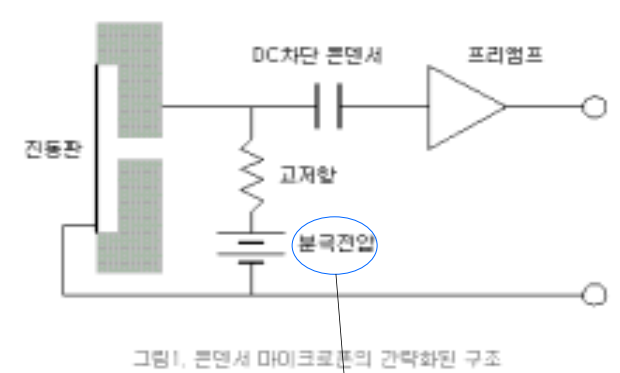


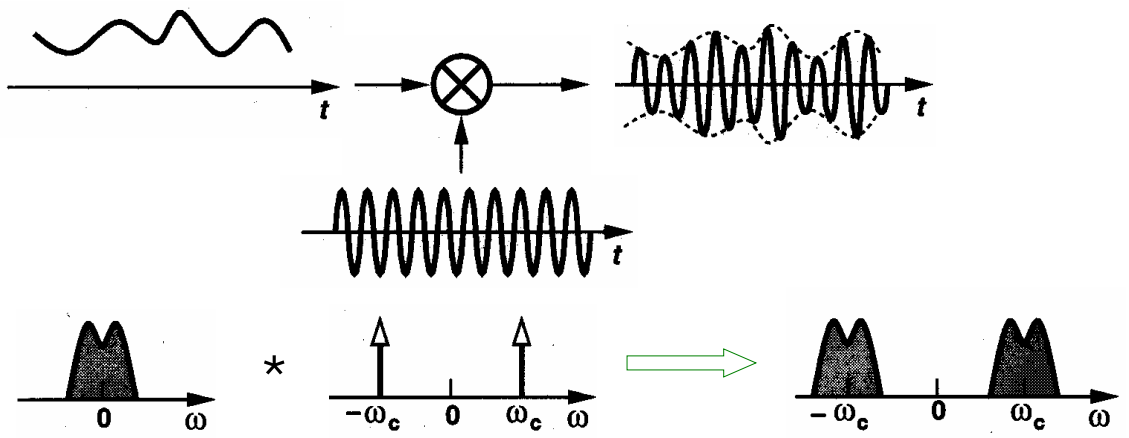
그림1. 콘덴서 마이크론의 간략화된 구조

(100~400 V)

Electret Condenser Microphone  
 : electret ( )  
 가 .

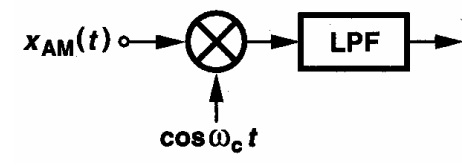
1. Amplitude Modulation (AM)

Amplitude Modulation BB signal:  $x_{BB}(t)$   $\xrightarrow{AM}$   $x_{AM}(t) = A_c[1 + mx_{BB}(t)] \cos \omega_c t$

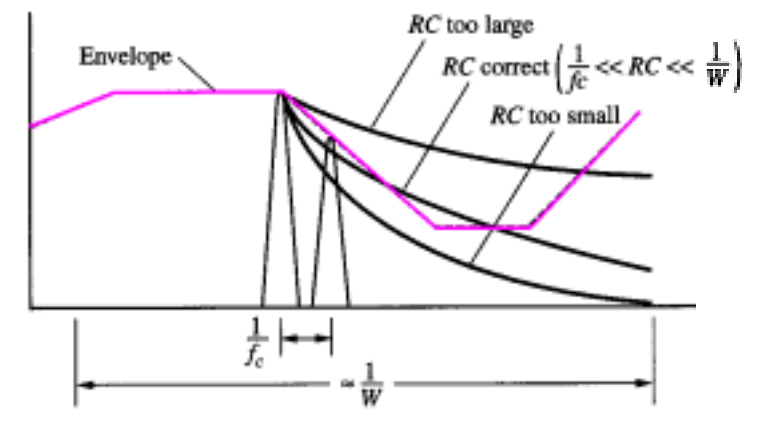
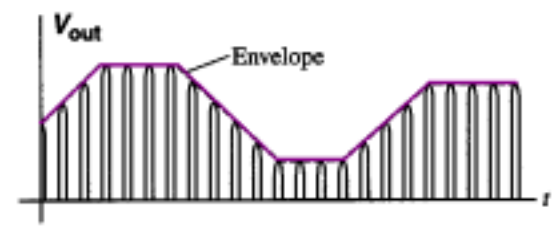
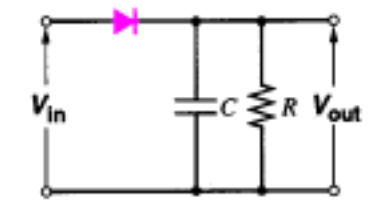
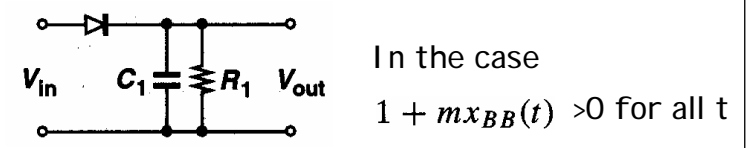


Demodulation:

(a) Coherent demodulation



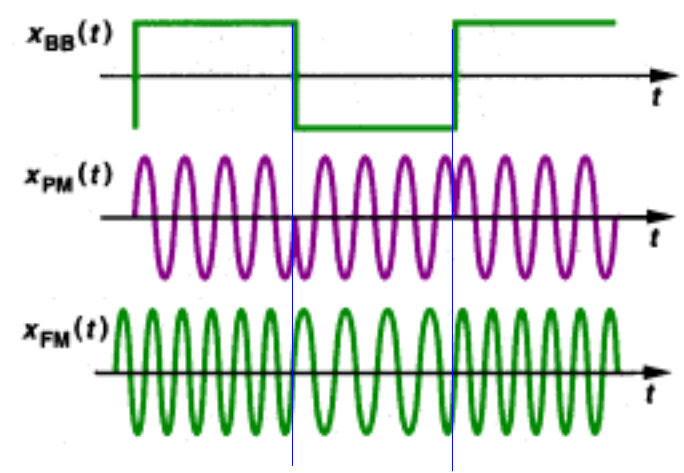
(b) Noncoherent demodulation - Envelope detection



2 Phase and Frequency Modulation

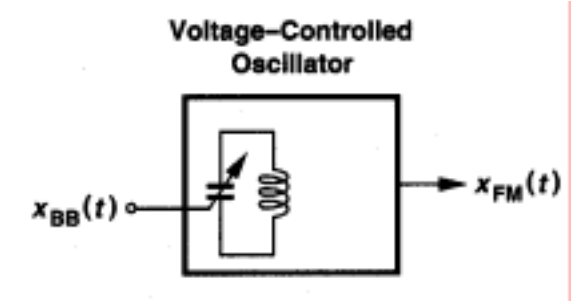
Phase Modulation (PM):  $x_{PM}(t) = A_c \cos[\omega_c t + mx_{BB}(t)]$

Frequency Modulation (FM):  $x_{FM}(t) = A_c \cos[\omega_c t + m \int_{-\infty}^t x_{BB}(t) dt]$

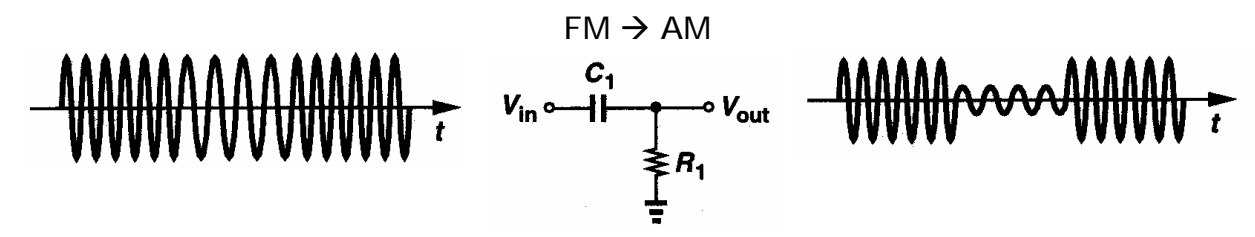


2.2 Phase and Frequency Modulation

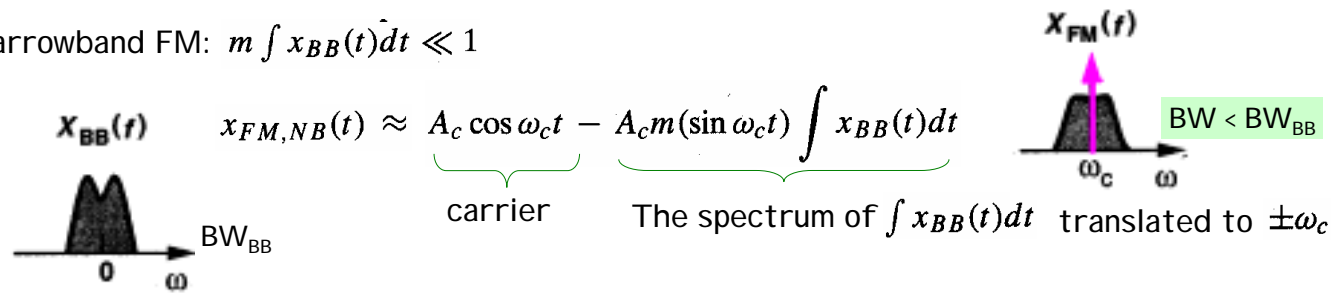
Frequency Modulator using a varactor diode



Demodulator using a high-pass filter (i.e., a differentiator)



Narrowband FM:  $m \int x_{BB}(t) dt \ll 1$



For a special case:  $x_{BB}(t) = A_m \cos \omega_m t$

$$x_{FM}(t) = A_c \cos[\omega_c t + m \int_{-\infty}^t x_{BB}(t) dt]$$

$$= A_c \cos[\omega_c t + (mA_m/\omega_m) \sin \omega_m t]$$

$\beta = mA_m/\omega_m \ll 1$

$$x_{FM,NB}(t) \approx A_c \cos \omega_c t - A_m A_c \frac{m}{\omega_m} \sin \omega_c t \sin \omega_m t$$

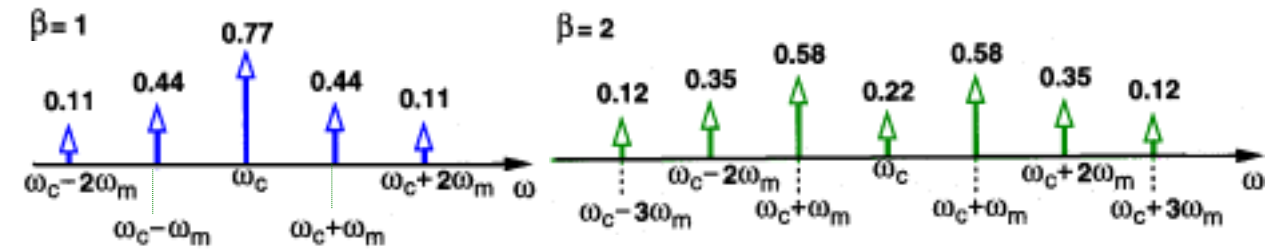
$$= A_c \cos \omega_c t - \frac{A_m A_c m}{2\omega_m} \cos(\omega_c - \omega_m)t + \frac{A_m A_c m}{2\omega_m} \cos(\omega_c + \omega_m)t.$$

Wideband FM:  $x_{FM}(t) = A_c \cos[\omega_c t + m \int_{-\infty}^t x_{BB}(t) dt]$

$$x_{BB}(t) = A_m \cos \omega_m t \rightarrow x_{FM}(t) = A_c \cos[\omega_c t + (mA_m/\omega_m) \sin \omega_m t]$$

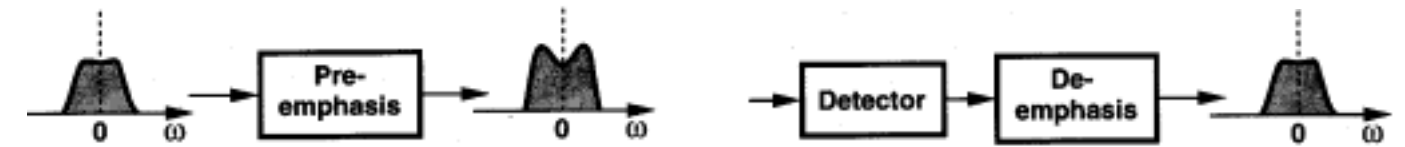
$$x_{FM}(t) = A_c \sum_{n=-\infty}^{+\infty} J_n(\beta) \cos(\omega_c + n\omega_m)t \quad \beta = mA_m/\omega_m$$

$J_n(\cdot)$  :  $n$ -th order Bessel function of the 1-st kind



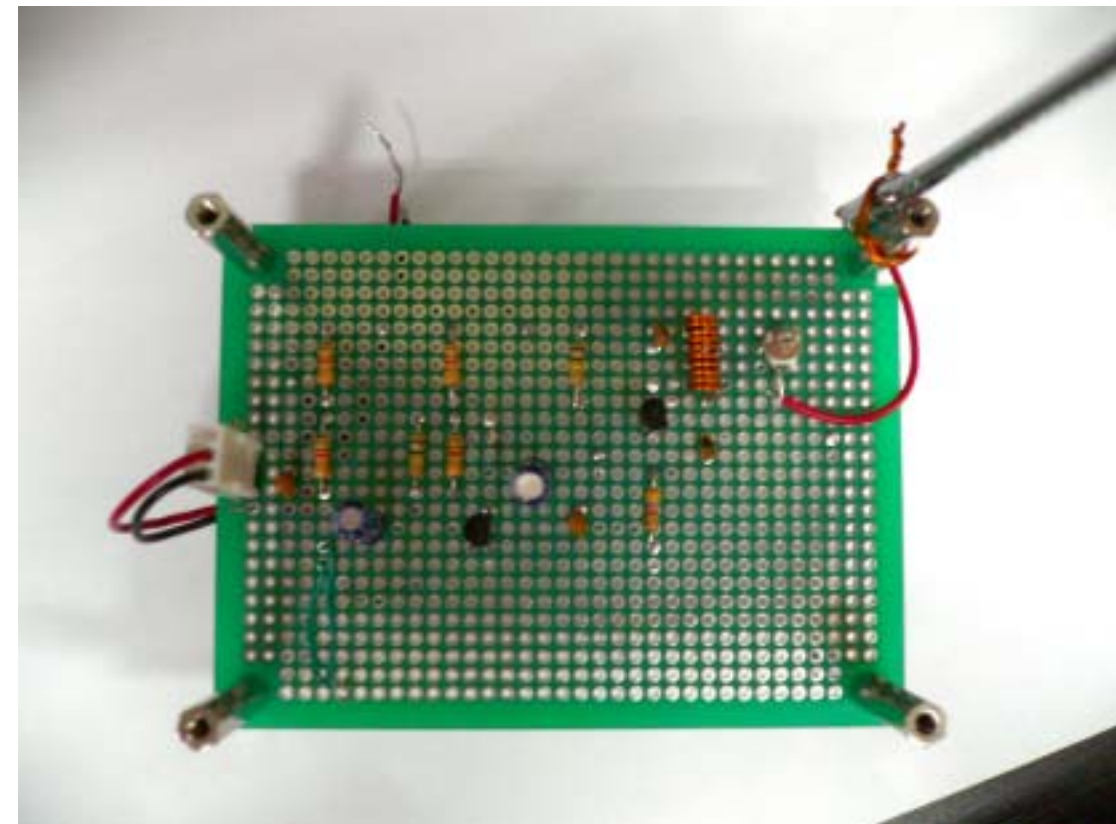
Bandwidth (Carson's Rule):  $B_{FM} \approx 2(\beta + 1)B_{BB}$  — BW that containing 98% of the signal power

Preemphasis & Deemphasis:



Pre-Lab (5 26 ):

1. FM monopole 가
2. monopole FM 가 가?
3. FM
4. air-coil
5. Condenser Microphone



Pre-Lab(6 2 ):

1. monopole FM (polarization) 가?
2. FM 가?
3. (pre-emphasis, de-emphasis)
4.  $n$ -th order Bessel function of the 1-st kind

In-Lab:

1. base AC TR
2. ( air-coil tuning 가 ) 가
3. 3.1 DC bias / ( ) 3.2
4. FM transmitter air-coil tuning
- 5.

Post-Lab: (6 16 )

1. Pre-Lab In-Lab
2. 가? ( , multi-user, ...)
3. 가?
4. 가 ? (artwork, parasitic effect, ...)
5. FM PLL
6. FM
7. 가
8. ( business model , marketing , 가 , ....) 가

